

Sample Exam No. 2 Solutions

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a) Kinetic Energy $K = 1/2 M_1 \dot{y}_1^2 + 1/2 M_2 \dot{y}_2^2$.

b) Potential Energy $P = 1/2 K_1 y_1^2 + 1/2 K_2 (y_2 - y_1)^2$.

c) $L = K - P = 1/2 M_1 \dot{y}_1^2 + 1/2 M_2 \dot{y}_2^2 - 1/2 K_1 y_1^2 - 1/2 K_2 (y_2 - y_1)^2$

$$\frac{\partial L}{\partial \dot{y}_1} = M_1 \dot{y}_1; \quad \frac{d}{dt} \frac{\partial L}{\partial \dot{y}_1} = M_1 \ddot{y}_1; \quad \frac{\partial L}{\partial y_1} = -K_1 y_1 + K_2 (y_2 - y_1)$$

$$\frac{\partial L}{\partial \dot{y}_2} = M_2 \dot{y}_2; \quad \frac{d}{dt} \frac{\partial L}{\partial \dot{y}_2} = M_2 \ddot{y}_2; \quad \frac{\partial L}{\partial y_2} = -K_2 (y_2 - y_1).$$

Euler-Lagrange Equations

$$M_1 \ddot{y}_1 + K_1 y_1 - K_2 (y_2 - y_1) = -B_1 \dot{y}_1$$

$$M_2 \ddot{y}_2 + K_2 (y_2 - y_1) = u - B_2 \dot{y}_2$$

or

$$M_1 \ddot{y}_1 + B_1 \dot{y}_1 + K_1 y_1 - K_2 (y_2 - y_1) = 0$$

$$M_2 \ddot{y}_2 + B_2 \dot{y}_2 + K_2 (y_2 - y_1) = u.$$

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$$\ddot{\theta}_1 + (3 \sin \theta_1) \dot{\theta}_2 + \dot{\theta}_1 \dot{\theta}_2 + \sin \theta_2 = \tau_1 + \tau_2$$

$$\ddot{\theta}_2 - (2 \sin \theta_1) \dot{\theta}_1 - \dot{\theta}_1 \dot{\theta}_2 = \tau_2.$$

In matrix form we can write this as

$$M(\theta) \ddot{\theta} + h(\theta, \dot{\theta}) = B \tau$$

where

$$M(\theta) = \begin{bmatrix} 1 & 3 \sin \theta_1 \\ -2 \sin \theta_1 & 1 \end{bmatrix}$$

$$h(\theta, \dot{\theta}) = \begin{bmatrix} \dot{\theta}_1 \dot{\theta}_2 + \sin \theta_2 \\ -\dot{\theta}_1 \dot{\theta}_2 \end{bmatrix}$$

$$B = \begin{bmatrix} 1 & 1 \\ 0 & 1 \end{bmatrix}$$

Therefore, by inspection, we see that an inverse dynamics control law is

$$\tau = B^{-1}\{M(\theta)a + h(\theta, \dot{\theta})\}.$$

Carrying out the calculations leads to

$$\begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = \begin{bmatrix} 1 & -1 \\ 0 & 1 \end{bmatrix} \left\{ \begin{bmatrix} 1 & 3\sin\theta_1 \\ -2\sin\theta_1 & 1 \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \end{bmatrix} + \begin{bmatrix} \dot{\theta}_1\dot{\theta}_2 + \sin\theta_2 \\ -\dot{\theta}_1\dot{\theta}_2 \end{bmatrix} \right\}$$

or

$$\tau_1 = (1 + 2\sin\theta_1)a_1 + (3\sin\theta_1 - 1)a_2 + 2\dot{\theta}_1\dot{\theta}_2 + \sin\theta_1$$

$$\tau_2 = -(2\sin\theta_1)a_1 + a_2 - \dot{\theta}_1\dot{\theta}_2.$$

b) For

$$\ddot{\theta}_1 = a_1$$

$$\ddot{\theta}_2 = a_2$$

we can use

$$a_1 = -2\zeta_1\omega_1\dot{\theta}_1 - \omega_1^2\theta_1 + r_1$$

$$a_2 = -2\zeta_2\omega_2\dot{\theta}_2 - \omega_2^2\theta_2 + r_2$$

where r_1, r_2 are reference input signals. With $\zeta_1 = \zeta_2 = 1$; $\omega_1 = \omega_2 = 10$ we have

$$a_1 = -20\dot{\theta}_1 - 100\theta_1 + r_1$$

$$a_2 = -20\dot{\theta}_2 - 100\theta_2 + r_2.$$

- 3 Without the feedforward transfer function $F(s)$ the closed loop system is $\frac{GH}{1+GH}$ where $G(s) = \frac{1}{s^2+4s}$ and $H(s)$ is a PD compensator $H(s) = K_p + K_v s$. Carrying out the calculations leads to

$$\frac{GH}{1+GH} = \frac{K_p + K_v s}{s^2 + (4 + K_v)s + K_p}.$$

a) The closed loop characteristic polynomial is $s^2 + (4 + K_v)s + K_p$. Therefore

$$K_p = \omega^2$$

$$4 + K_v = 2\zeta\omega$$

with $\zeta = 1$, $\omega = 12$ this leads to

$$K_p = 144$$

$$K_v = 20.$$

b) To track a time-varying reference we know that we should choose

$$F(s) = \frac{1}{G(s)} = s^2 + 4s.$$

This leads to the feedforward signal

$$\left(\frac{d^2}{dt^2} + 4 \frac{d}{dt} \right) \cos 3t$$

$$= -9 \cos 3t - 12 \sin 3t.$$

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$$\dot{x}_1 = x_2$$

$$\dot{x}_2 = -x_1 - x_1^2 x_2.$$

a) The equilibrium points are found from

$$\begin{aligned} x_2 &= 0 \\ -x_1 - x_1^2 x_2 &= 0 \end{aligned} \Rightarrow \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}.$$

b) With $V = x_1^2 + x_2^2$ we have

$$\begin{aligned} \dot{V} &= 2x_1 \dot{x}_1 + 2x_2 \dot{x}_2 \\ &= 2x_1 x_2 + 2x_2 (-x_1 - x_1^2 x_2) \\ &= -2x_1^2 x_2^2 < 0 \end{aligned}$$

Therefore $V(\mathbf{x}) > 0$ for $\mathbf{x} \neq \begin{pmatrix} 0 \\ 0 \end{pmatrix}$ and $\dot{V}(\mathbf{x}) < 0$.

Hence the origin is an asymptotically stable equilibrium.